
In-Situ Testing of Gas Orifice Meters

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Overview

- ▼ Why do we do *in-situ* testing
- ▼ Test Equipment
- ▼ Design Considerations
- ▼ Summary

Elements of a *Differential Producer*

- ▼ Primary Element--mostly steel; subjected to pressure, temperature, and flow velocity, but no electronics
- ▼ Sensing Element--electronics and exotic metals; subjected to pressure and temperature, but not flow; generates electronic signals or pen movements.
- ▼ Recording Element--Electronics or pen & ink; only sees electronic signals or pen movements
- ▼ Differential Producers are *Inferential Devices*
 - Assuming **all conditions match reference conditions** you can use *Bernoulli's Equation* to infer a flow rate from a differential pressure across a known restriction

Assumptions in Calculations

- | | |
|--|---|
| ▼ Constant density at each snapshot | ▼ Fluid properties known and constant for each snapshot |
| ▼ No friction | ▼ Enough friction to dampen swirl |
| ▼ Tube is straight and level | ▼ Press and Temp known |
| ▼ Gas does no work | ▼ Tube roughness in narrow range |
| ▼ Flow profile matches power law | ▼ Plate condition meets specs |
| ▼ Single phase flow | ▼ Plate bore concentric to tube bore |
| ▼ Atmospheric pressure known precisely | |

Measurement *System Accuracy*

- ▼ Each element of a measurement system is:
 - manufactured to close tolerances
 - inspected by the manufacturer and purchaser
 - installed to precise specifications
- ▼ After all that, what can still be wrong?

What can be wrong with a new installation?

- ▼ Flow profile
- ▼ Backwards plate
- ▼ Beta Ratio
- ▼ Incorrect station parameters
- ▼ Non-rigid mounting

Flow Profile

- ▼ Problem
 - 25% of flow not in center
20% of pipe
 - Error can be low by 5% or more
- ▼ How to prevent it
 - Upstream piping
 - Flow Conditioners and/or Straightening vanes
- ▼ How to detect it
 - *In Situ* Testing



Backwards Plate

- ▼ Problem
 - Leading edge shaped like a venturi
 - Reading can be as much as 26% low
- ▼ How to prevent it
 - Attention to details
- ▼ How to detect it
 - *In Situ* testing

Beta Ratio

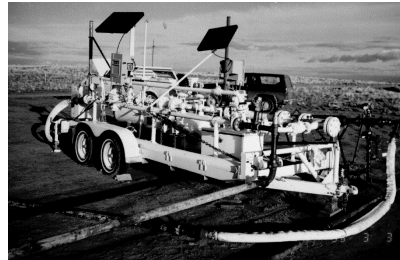
- ▼ Problem:
 - Uncertainty in gas measurement is controlled to a large extent by beta ratio
 - » Less than 0.3, uncertainty is a function of edge sharpness and concentricity
 - » Greater than about 0.62, it increases very quickly
 - Combined error can be 7%
- ▼ How do you prevent it
 - Proper station design
- ▼ How do you detect how “uncertainty” equates to “error”
 - *In Situ* Testing

Incorrect station parameters

- ▼ Problem
 - Any of the parameters from gas analysis to Tube ID will affect the conversion of dP, P, and T to flow rate
 - Combined error can be over 10%
- ▼ What can you do to prevent errors
 - Double check original input (two people)
- ▼ What can you do to detect errors
 - Verify all parameters each calibration
 - *In Situ* Testing

Non-Rigid Mounting

- ▼ Problem
 - The gas does work (reducing dP)
 - up to 15% error
- ▼ How to prevent
 - Independent braces
 - Use hold-down bolts
- ▼ How to detect
 - Inspection after installation
 - *In-Situ* testing



Installation Verification

- ▼ To insure that a new station meets its potential:
 - Install all the parts at their final location
 - Use “normal” gas at “normal” temperature and pressure
 - Design a test manifold that ensures that all gas goes through the test skid after the new station
 - Use a certified test skid

When to Test

- ▼ As part of station commissioning process
- ▼ Regularly on very large volume stations
- ▼ Regularly on particularly erosive/corrosive or dirty applications
- ▼ When routine plate inspections point to a problem

Test Equipment

- ▼ Uncertainty
- ▼ Calibrated Differential Producer
- ▼ Proportional devices with provers
 - Turbine meters
 - Vortex-shedding meters
- ▼ Inferential vs. Proportional devices
- ▼ Calibration methods

Uncertainty

- ▼ Uncertainty means “you don’t know”
- ▼ No conclusions can be drawn from data beyond the uncertainty range, for example:
 - If a calibration device is stated to be $\pm 0.5\%$
 - Your tested device is off by 0.6%
 - Actual results are 0.1-1.1% and the meter has a bias high
- ▼ Consequently:
 - a calibration device can only certify a calibrated device to within twice its uncertainty (i.e., a 0.25% device must be used to calibrate a 0.5% device)
 - Midpoint of a confidence range must fall within the dead-zone around zero (i.e., the center of a 90% confidence range from a 0.5% skid must be in the range -0.5-0.5%)

Calibrated Differential Producer Skid

- ▼ As long as:
 - The test manifold has positive isolation between inlet and outlet
 - Sensing elements on test skid are calibrated before every test
 - Orifice plates on test skid are inspected before and after every test
 - Tube on test skid is inspected quarterly
 - Recording elements are verified against a calculation standard frequently
 - The skid is certified against a primary standard annually to be within $\pm 0.5\%$
- ▼ A properly designed Differential Producer Skid can be used to certify a station is $\pm 1.0\%$

Proportional Devices

- ▼ All have some moving part that is proportional to mass flow rate (motion can be gross like a turbine rotor or microscopic like the vibration frequency of a vortex)
- ▼ They are all prone to:
 - Foul in dirty fluid (20 mils of paraffin on a turbine blade caused the reading to be 2% low in one test against a primary standard)
 - Have bearing or vibration-sensor wear that is not obvious on recording element
- ▼ A Proportional Skid must be calibrated against a primary standard before and after each station test

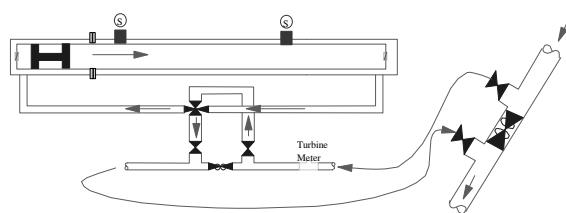
Inferential vs. Proportional

- | <u>Inferential</u> | <u>Proportional</u> |
|---|--|
| <ul style="list-style-type: none">▼ Pros<ul style="list-style-type: none">– No moving parts– Well understood in field– Very rugged– Useable in dirtier fluids▼ Cons<ul style="list-style-type: none">– Narrow rangability– “Flow” measurement unrelated to fluid density | <ul style="list-style-type: none">▼ Pros<ul style="list-style-type: none">– Good rangability– Flow measurement is directly related to mass flow rate▼ Cons<ul style="list-style-type: none">– Moving parts prone to fouling and wear– Must be recalibrated before and after each use– Should not be used with dirty fluids |

Calibration Methods

- ▼ Piston Prover
- ▼ Sonic nozzle
- ▼ Primary standards not discussed in this paper:
 - Weigh tanks
 - High pressure Bell Prover

Piston Prover



- ▼ Piston used to quickly develop “k-factor” for turbine meter
- ▼ Turbine meter is used to prove station being tested
- ▼ After test, turbine can be re-proven

Piston Prover Design Considerations

- ▼ Piston run times related to flow by:
 - Precise displacement volume
 - Exact duration of travel between detector switches
 - Exact count of piston round trips
- ▼ Obstacles to use in gas
 - No U.S. standards exist for piston provers in compressible flow (some European countries have adopted procedures and ISO is evaluating)
 - Gas pressure must increase to overcome piston inertia
 - Fairly small volume capacity
- ▼ Techniques to overcome obstacles
 - New correlations based on equations of state
 - Bi-directional pistons
 - Fast-acting, electronically operated diverter valves
 - Acceleration/deceleration regions before/after measured volume
 - Use Piston to prove turbine and turbine to prove installed station

Sonic Nozzle

- ▼ Under most conditions, a compressible fluid is limited to speeds less than or equal to the speed of sound
- ▼ Sonic (or Critical Flow) nozzles use a substantial pressure drop to force the gas to the speed of sound
 - With an open-ended pipe sonic velocity is reached when downstream pressure (psia) is less than 1/2 upstream pressure
 - Properly designed convergent/divergent nozzles can reduce this to about 20% pressure drop
- ▼ With careful measurement of upstream pressure, temperature, and gas composition; very accurate (about $\pm 0.25\%$) mass flow measurement is possible so volumes can be accurately determined

Sonic Nozzle Limitations

- ▼ They require a large differential pressure, so:
 - It can be difficult to get the gas back into the line
 - If hydrocarbon gas is discharged to atmosphere, care must be taken to avoid an explosive atmosphere
 - Liquids can drop out of gas
 - Temperature drop can cause hydrates to freeze
- ▼ They are not effective in multi-phase flow
- ▼ Calculations require careful evaluation of:
 - Atmospheric pressure
 - Upstream temperature and pressure
 - Density
 - Compressibility

Sonic Nozzle Use in *In-Situ* Testing

- ▼ Considerations
 - Use dry air or non-flammable gas as test fluid
 - Ensure that operating personnel are careful, competent, and observant
 - Verify that atmospheric pressure and gas composition are the same in EFM unit as in test-facility computer
 - Verify that EFM unit uses the same Temp and Pressure base as the test facility
 - Verify that EFM unit uses the same compressibility calculation as test facility
- ▼ With proper diligence, a sonic nozzle can be used to certify that the differential producers on a test skid are accurate to $\pm 0.5\%$ of volumetric flow rate

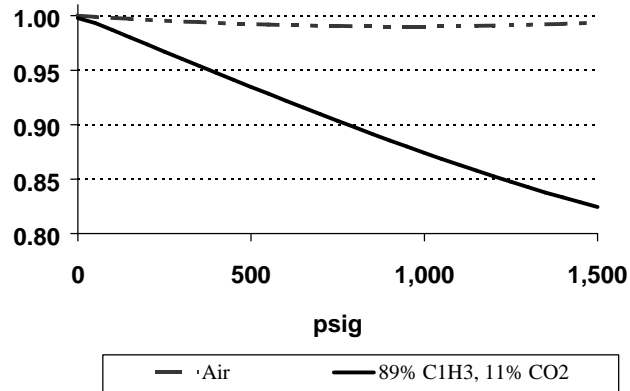
Test Skid Design Considerations

- ▼ Flow conditioning
- ▼ Capacity and Rangeability
- ▼ Operating pressures and temperatures
- ▼ Flexibility
- ▼ Data Capture
- ▼ Transportability

Why do we need Flow Conditioning?

- ▼ Any device used on a test skid will be sensitive to flow profile problems
- ▼ Confined-space piping on test skid will contribute to poor flow profiles
- ▼ Swirl and asymmetry cause flow-rate errors that are related to compressibility and density
- ▼ Flow conditioners with straightening vanes are required to get repeatable results that can be transferred from one type of gas to another

Changes in Compressibility



Capacity and Rangeability

- ▼ Skid capacity should be
 - Large enough to handle max expected volume
 - Small enough to be within design conditions for min volume
 - Appropriate to keep sensing elements within 10-90% of calibrated range
- ▼ Example
 - A differential producer has a range of about 6:1 (assuming arbitrary limitations on beta-ratio of 0.3-0.6 and dP of 45-105")
 - A skid with one 3-inch and one 6-inch tube (and the piping to run them in parallel) has a range of almost 39:1 (with the same limitations)

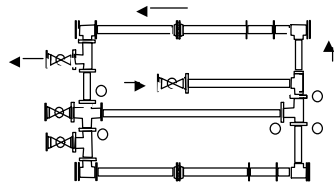
Operating Pressures & Temperatures

- ▼ The test skid (excluding hoses) should be designed to handle 150% of design pressure on highest design-pressure station in the operation
- ▼ Increase hydrostatic test pressure to compensate for the lowest ambient temperature expected
- ▼ Hoses should be:
 - Designed for most-likely pressures and temperatures
 - Labeled with MAOP
 - Tested to 150% of MAOP annually (hold test for 24 hours)

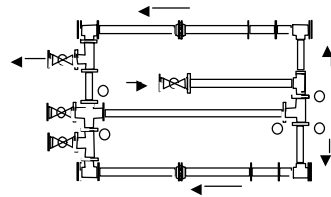
Flexibility

- ▼ The test skid should be able to:
 - Use one meter to evaluate one stream
 - Use some combination of skid meters in parallel for larger streams
 - Simultaneously evaluate multiple flow streams
 - Re-measure a given stream multiple times
- ▼ Possible reasons to re-measure
 - Compare one meter to another to quickly evaluate “calibration”
 - Evaluate impact of damaged plates
- ▼ Streams must be positively isolated from each other
 - Double-Block-and-Bleed valves
 - Spectacle blinds

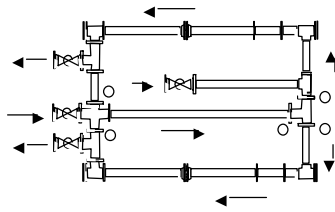
Flexible Flow



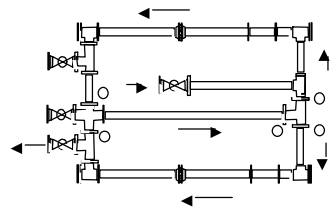
Normal Flow



Parallel Flow



2-Stream



Serial Flow

Data Capture

- ▼ Types of data
 - Prover reports
 - Flow Parameter reports
 - Volume reports
- ▼ Data should be available on both paper and ASCII files
- ▼ Data should be able to accumulate/summarize data over flexible time frames
- ▼ For each time frame, capture at least:
 - Cumulative volume for period
 - Average flow rate during period
 - Instantaneous flow rate at end of period
 - Average and snapshot temperature, dP, and static pressure for each calc

Data Analysis

- ▼ At least 30 time periods must be used, any number greater than 30 is acceptable
- ▼ It is better to use cumulative gas for each time period than to use flow rates
- ▼ Calculate:

$$\text{Error} = \frac{\sum \text{Skid Volume} - \sum \text{Station Volume}}{\sum \text{Skid Volume}} \times 100$$

- Total error should be less than 1%
- Error for individual time periods should be computed and checked for:
 - » Standard deviation of errors
 - » Mean error
 - » Count of periods above and below zero (worse than 60-40% distribution indicates a bias when n>30)

$$90\% \text{ Confidence} = \frac{1.65 \times \text{Standard Deviation}}{\sqrt{\text{Sample Count}}} = \text{CONFIDENCE}(0.10, \text{Std Dev}, n)$$

Data Analysis Example

	Acceptable Range	Meter 1	Meter 2
Total Error	-1% to 1%	-0.88%	-0.32%
Mean Error		-0.99%	-0.07%
Std Deviation		0.58%	0.42%
90% confidence	-1% to 1%	-1.10% to -0.88%	-0.15% to 0.0%
Count < 0	32-48	75	44
Count > 0	32-48	5	36
Conclusion		Bias low	Accurate Meas

- ▼ Notes:
 - Total error and mean error values -0.5 to 0.5% mean “accurate values” no conclusions can be drawn about where a number falls in that range
 - Midpoint of 90% confidence range must fall between -0.5 to 0.5% on passing tests
 - Rule of thumb count range
 - » 30 < n < 100 ==> acceptable range = 0.4n to 0.6n
 - » n > 100 ==> acceptable range = 0.45n to 0.55 n

Transportability

- ▼ Considerations
 - Weight
 - Width (limited to about 8-feet)
 - Fitting all piping/equipment onto skid
- ▼ Non-negotiable items
 - Isolation between streams must be positive (either block and bleed or spectacle blinds)
 - Differential producers must have dual-chamber fittings
 - Flow profile-isolating conditioner must be installed upstream of each station

Transportability Options

- ▼ Truck Mounting
 - Larger weight-carrying capacity
 - Considerable flexibility in skid size
 - Leveling can be tricky
 - Transportation for driver can be a problem after hook-up
 - Bed height can be a problem with operations personnel
- ▼ Trailer mounting
 - Many weight/size compromises needed
 - Axles and tongue (or 5th wheel) need to be matched to weight
 - Less expensive than truck-mounted
- ▼ Cargo
 - Least expensive
 - Least convenient for moving

Summary

- ▼ *In-Situ* testing is both necessary and practical
- ▼ It ensures
 - The measurement system works together
 - Large stations continue to work
 - Stations in dirty/corrosive/erosive streams continue to work
- ▼ Skid certification:
 - Proportional skids should have a built-in prover
 - Differential-producer skids should be calibrated periodically
- ▼ The skid must be designed to
 - be transported, leveled, and connected to the process gas
 - allow a wide variety of flows
 - work with expected fluid pressures, temperatures, and fluid qualities
 - capture data consistent with installed equipment